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Glossary

Application Site	The area within the red line Planning Boundary comprising the Onshore Transmission Works (OnTW), as defined.
dB (decibel)	The scale on which sound pressure level is expressed. It is defined as 20 times the logarithm of the ratio between the root-mean-square pressure of the sound field and a reference pressure (2×10^{-5} Pa).
dB(A)	A-weighted decibel. This is a measure of the overall level of sound across the audible spectrum with a frequency weighting ('A' weighting) to compensate for the varying sensitivity of the human ear to sound at different frequencies.
EIA Report	Report presenting the findings of the Environmental Impact Assessment (EIA).
L_{Aeq}	L_{Aeq} is defined as the notional steady sound level which, over a stated period of time, would contain the same amount of acoustical energy as the A-weighted fluctuating sound measured over that period.
Onshore Substation	The electrical substation comprising of all the equipment and associate infrastructure required to enable connection to the electrical transmission grid.
Onshore Transmission Works (OnTW)	All proposed works within the Application Site, typically including the Onshore Substation, cables transition pits, cable jointing pits, underground electricity transmission cables connecting to the Onshore Substation and further underground cables required to facilitate connection to the national grid. This includes all permanent and temporary works required. See <i>Chapter 5: Description of Development</i> for full details.
Planning Boundary	The red line application boundary containing the Onshore Transmission Works (OnTW), as defined.
Scoping Opinion	The Scoping Opinion adopted by ELC as to the scope and information to be provided in support of an application for the OnTW, as defined.

Abbreviations and Acronyms

dB	Decibel
ELC	East Lothian Council
L_{Aeq,T}	Predicted Sound Level
L_{Ar,T}	Predicted Rating Level, dB
L_p	Sound Pressure Level
L_w	Sound Power Level
OnTW	Onshore Transmission Works

3D Noise and Landscape Assessment without the Bund to the North of Atholl View

3D.1 Background

- 1 This appendix details the results of an indicative noise and visual impact assessment of the potential impacts associated with the operation of the Onshore Transmission Works (OnTW), in the event that the earth bund located to the south of the Application Site (north of Atholl View) is no longer in place. This work has been carried out following a request from East Lothian Council (ELC) in their Scoping Opinion (*Appendix 3A*, Volume 2) and in subsequent responses on this matter from ELC (see *Appendix 3B-3C*, Volume 2).
- 2 It is ICOL's understanding that the bund to the north of Atholl View is well established and there are no current proposals to remove this bund, and as such it is considered representative of the baseline and is likely to remain in place for the operational life of the OnTW.
- 3 In order to comply with ELC's requests ICOL has provided this additional assessment, although ICOL do not consider this part of the Environmental Impact Assessment (EIA) for the OnTW.
- 4 This assessment should be treated as illustrative and if any proposal to remove or modify the bund is submitted to ELC there will be a requirement on the applicant of that project to assess the associated impacts.

3D.2 Noise Assessment

3D.2.1 Effects of Operation and Maintenance

- 5 This section presents an indicative assessment of the potential noise impact associated with the operation of the OnTW, in the event that the earth bund located to the south of the Application Site (north of Atholl View) is not in place. The assessment methodology is in line with that presented in *Chapter 10: Noise and Vibration*, but presents alternative results as per a request from ELC.
- 6 The prediction of operational noise has been undertaken using the CadnaA[®] noise model and the calculation algorithms set out in ISO 9613-2:1996. The noise model has assumed the following appropriate assumptions:
 - Downwind propagation, i.e. a wind direction that assists the propagation of sound from source to receptor;
 - A ground absorption factor of 0.5 (mixed ground);
 - A reflection factor of 2;
 - A daytime receptor height of 1.5 m to represent a ground floor (living room) window; and
 - A night-time receptor height of 4 m to represent a first floor (bedroom) window.
- 7 Barrier attenuation from local topography has been incorporated into the CadnaA[®] noise model using OS '*Terrain 5'* data; however, the existing earth bund to the south of the

Application Site and to the north of the residential properties on Atholl View has not been included. It should be noted that an assumption should be made that the theoretical removal of the bund north of Atholl View would involve removal of the bund to ground level. The model accounts for the proposed landscape mitigation plan; however, attenuation from man-made structures has not been considered.

- 8 The specific sound sources associated with the Onshore Substation are presented in Table 1. The data has been based on the proposed layout (Figure 5.9 in *Chapter 5: Description of Development*); however, it should be noted that the layout and design of the Onshore Substation is not yet finalised and is therefore only indicative at this stage.
- 9 The assessment has been based on currently available sound level information associated with similar developments, whereby it is considered that there would be embedded mitigation incorporated into the design. In this respect, and for the purposes of the assessment, it has been assumed that some components of the Onshore Substation would be enclosed, namely the transformer tanks and shunt reactor tanks. These enclosures would provide 20 dB(A) attenuation to the sound power levels of these sources.

Table 3D. 1: Specific Sound Sources – Embedded Mitigation only

Specific Sound Source	Sound Power Level (L_w) or Sound Pressure Level (L_p)	Number of Each
Shunt Reactors – Tanks (SHR1, SHR2, SHR3 & SHR4)	$L_w = 72 \text{ dB(A) }^*$	4
Shunt Reactors – Coolers (SHR1, SHR2, SHR3 & SHR4)	$L_w = 84 \text{ dB(A)}$	4
Transformers – Tanks (SGT1 & SGT2)	$L_w = 75 \text{ dB(A) }^*$	2
Transformers – Coolers (SGT1 & SGT2)	$L_w = 87 \text{ dB(A)}$	2
MSR Reactor 1; MSR Reactor 2	$L_p = 65 \text{ dB(A) at 2 m}$	3 reactors per circuit (6 in total)
SVC Phase Reactors (Reactor 1 & Reactor 2)	$L_p = 62 \text{ dB(A) at 2 m}$	2
SVC Coolers	$L_w = 90 \text{ dB(A)}$	2
SVCPLUS Building – Air Conditioning (various)	$L_p = 47 \text{ dB(A) at 10 m}$ $L_p = 51 \text{ dB(A) at 10 m}$	1 7

Specific Sound Source	Sound Power Level (L_w) or Sound Pressure Level (L_p)	Number of Each
Filter Building – Air Handling Units	$L_w = 85$ dB(A)	6
SVC Control Building – Condenser Units (various)	$L_w = 76$ dB(A)	5
	$L_w = 81$ dB(A)	3
	$L_w = 62$ dB(A)	1
*Attenuation (20 dB(A)) provided to these sound sources by acoustic enclosures		

- 10 The specific sound levels, due to the operation of the OnTW and without the effect of the earth bund, have been presented as indicative to reflect the theoretical nature of the assessment at the closest receptors using the CadnaA® noise model. The results are presented in Table 2 and are rounded to the nearest decibel (dB). These predicted sound levels are representative of the worst case, whereby it has been assumed that all the identified sound sources are operating simultaneously and continuously, and on a 24/7 basis. These are therefore the highest predicted ambient noise levels expected during operation of the OnTW.

Table 3D. 2: Indicative Operational Sound Levels, dB – Embedded Mitigation only

NSR ID	NSR Name	Assessment Period	Predicted Sound Level, $L_{Aeq,T}$
NSR01	No. 1 & 2 Edinburgh Road	Daytime	28
		Night-time	28
NSR02	West Harbour Road	Daytime	25
		Night-time	26
NSR03	Cockenzie House & Gardens	Daytime	23
		Night-time	24
NSR04	Hawthorn Terrace	Daytime	29
		Night-time	30
NSR05	The Antiquaries	Daytime	24
		Night-time	25
NSR06	Atholl View	Daytime	29
		Night-time	32

NSR ID	NSR Name	Assessment Period	Predicted Sound Level, $L_{Aeq,T}$
NSR07	Appin Drive	Daytime	23
		Night-time	25
NSR08	Hawthorn Bank	Daytime	26
		Night-time	26

- 11 The acoustic character of each specific sound source, and the resulting sound penalty that would apply in accordance with BS4142:2014, is detailed in Table 3.

Table 3D. 3: Acoustic Characteristics of Specific Sound Sources

Specific Sound Source	Tonal Sound	Impulsive Sound	Intermittent Sound	Other Sound	Comment
Shunt Reactors – Tanks	Yes = 2 dB	No	No	No	At NSRs within 100 m (none identified), tones may be clearly perceptible (4 dB penalty), whilst at NSRs further afield, tones may be just perceptible (2 dB penalty). Reactors would run continuously.
Shunt Reactors – Coolers	No	No	No	No	Reactors would run continuously.
Transformers – Tanks	Yes = 2 dB	No	No	No	At NSRs within 100 m (none identified), tones may be clearly perceptible (4 dB penalty), whilst at NSRs further afield, tones may be just perceptible (2 dB penalty). Transformers would run continuously.

Specific Sound Source	Tonal Sound	Impulsive Sound	Intermittent Sound	Other Sound	Comment
Transformers – Coolers	No	No	No	No	Transformers would run continuously.
MSR Reactors	No	No	No	No	Reactors would run continuously.
SVC Phase Reactors	Possibly = 2 dB	No	No	No	At NSRs within 100 m (none identified), tones may be clearly perceptible (4 dB penalty), whilst at NSRs further afield, tones may be just perceptible (2 dB penalty). Reactors would run continuously.
SVC Coolers	No	No	Yes = 3 dB	No	On/off conditions, corresponding to maximum and minimum temperature settings.
SVCPLUS Building – Air Conditioning	Possibly = 2 dB	No	Yes = 3 dB	No	At NSRs within 100 m (none identified), tones may be clearly perceptible (4 dB penalty), whilst at NSRs further afield, tones may be just perceptible (2 dB penalty). On/off conditions, corresponding to maximum and minimum temperature settings.

Specific Sound Source	Tonal Sound	Impulsive Sound	Intermittent Sound	Other Sound	Comment
Filter Building – Air Handling Units	Possibly = 2 dB	No	Yes = 3 dB	No	At NSRs within 100 m (none identified), tones may be clearly perceptible (4 dB penalty), whilst at NSRs further afield, tones may be just perceptible (2 dB penalty). On/off conditions, corresponding to maximum and minimum temperature settings.
SVC Control Building – Condenser Units	Possibly = 2 dB	No	Yes = 3 dB	No	At NSRs within 100 m (none identified), tones may be clearly perceptible (4 dB penalty), whilst at NSRs further afield, tones may be just perceptible (2 dB penalty). On/off conditions, corresponding to maximum and minimum temperature settings.

- 12 Based on the data presented in Table 3, a penalty of +5 dB is applicable to the indicative predicted sound levels at the closest receptors in order to derive the corresponding rating levels.
- 13 The indicative rating levels have been compared to the measured background sound levels and assessed in accordance with BS4142:2014. The results are shown in Table 4, where the rating levels and the background sound levels have been rounded to the nearest dB.

Table 3D. 4: BS4142:2014 Indicative Assessment – Embedded Mitigation only

NSR ID	NSR Name	Assessment Period	Predicted Rating Level, dB L _{A,r,T} *	Background Sound Level, dB L _{A90}	Difference, dB
NSR01	No. 1 & 2 Edinburgh Road	Daytime	33	52	-19
		Night-time	33	35	-2
NSR02	West Harbour Road	Daytime	30	47	-17
		Night-time	31	36	-5
NSR03	Cockenzie House & Gardens	Daytime	28	47	-19
		Night-time	29	36	-7
NSR04	Hawthorn Terrace	Daytime	34	41	-7
		Night-time	35	29	+6
NSR05	The Antiquaries	Daytime	29	52	-23
		Night-time	30	30	0
NSR06	Atholl View	Daytime	34	34	0
		Night-time	37	26	+11
NSR07	Appin Drive	Daytime	28	42	-14
		Night-time	30	26	+4
NSR08	Hawthorn Bank	Daytime	31	52	-21
		Night-time	31	35	-4
* Predicted specific sound level (as per Table 2), plus a BS4142:2014 penalty of +5 dB					

- 14 It can be seen from Table 4 above, that the daytime and night-time rating level at the closest receptors is predicted to be below the corresponding background sound level at the majority of receptors, assuming that the earth bund is not in place.
- 15 However, at night-time and for NSR06 in particular (Atholl View), the rating level is predicted to be +11 dB above the measured night-time background sound level. BS4142:2014 states that *“a difference of around +10 dB or more is likely to be an indication of a significant adverse impact, depending on the context”*.
- 16 As such, mitigation has been *considered* with respect to the components of the Onshore Substation and their associated sound power levels. In addition to the Embedded Mitigation, which comprises acoustic enclosures for the shunt reactors and transformer tanks, *‘low noise’*

options are available for the shunt reactor coolers, transformer coolers and SVC coolers. This has been assumed within the CadnaA® noise model, whereby 10 dB(A) attenuation is expected to all coolers through the incorporation of 'low noise' components.

- 17 The resulting sound power levels or sound pressure levels (at a stated distance) are presented in Table 5 below.

Table 3D. 5: Specific Sound Sources – Embedded and Additional Mitigation

Specific Sound Source	Sound Power Level (L_w) or Sound Pressure Level (L_p)	Number of Each
Shunt Reactors – Tanks (SHR1, SHR2, SHR3 & SHR4)	$L_w = 72 \text{ dB(A) }^*$	4
Shunt Reactors – Coolers (SHR1, SHR2, SHR3 & SHR4)	$L_w = 74 \text{ dB(A) }^{**}$	4
Transformers – Tanks (SGT1 & SGT2)	$L_w = 75 \text{ dB(A) }^*$	2
Transformers – Coolers (SGT1 & SGT2)	$L_w = 77 \text{ dB(A) }^{**}$	2
MSR Reactor 1; MSR Reactor 2	$L_p = 65 \text{ dB(A) at 2 m}$	3 reactors per circuit (6 in total)
SVC Phase Reactors (Reactor 1 & Reactor 2)	$L_p = 62 \text{ dB(A) at 2 m}$	2
SVC Coolers	$L_w = 80 \text{ dB(A) }^{**}$	2
SVCPLUS Building – Air Conditioning (various)	$L_p = 47 \text{ dB(A) at 10 m}$ $L_p = 51 \text{ dB(A) at 10 m}$	1 7
Filter Building – Air Handling Units	$L_w = 85 \text{ dB(A)}$	6
SVC Control Building – Condenser Units (various)	$L_w = 76 \text{ dB(A)}$ $L_w = 81 \text{ dB(A)}$ $L_w = 62 \text{ dB(A)}$	5 3 1
*Attenuation (20 dB(A)) provided to these sound sources by acoustic enclosures ** 'Low noise' components, reducing sound power levels by 10 dB(A)		

18 The specific sound levels, due to the operation of the OnTW, without the bund, and incorporating embedded mitigation and additional ‘low noise’ mitigation options, have been predicted at the closest receptors and presented as indicative to reflect the theoretical nature of the assessment. The results are presented in Table 6 and are rounded to the nearest dB.

Table 3D. 6: Indicative Operational Sound Levels, dB - Embedded and Additional Mitigation

NSR ID	NSR Name	Assessment Period	Predicted Sound Level, L_{Aeq}
NSR01	No. 1 & 2 Edinburgh Road	Daytime	24
		Night-time	25
NSR02	West Harbour Road	Daytime	22
		Night-time	22
NSR03	Cockenzie House & Gardens	Daytime	20
		Night-time	20
NSR04	Hawthorn Terrace	Daytime	25
		Night-time	26
NSR05	The Antiquaries	Daytime	20
		Night-time	22
NSR06	Atholl View	Daytime	24
		Night-time	28
NSR07	Appin Drive	Daytime	20
		Night-time	21
NSR08	Hawthorn Bank	Daytime	22
		Night-time	22

19 Again, a penalty of +5 dB is applicable to the predicted specific sound level at the closest receptors in order to derive the corresponding rating levels. The rating levels have been compared to the measured background sound levels and assessed in accordance with BS4142:2014. The results are shown in Table 7, where the rating levels and the background sound levels have been rounded to the nearest dB.

Table 3D. 7: BS4142:2014 Indicative Assessment – Embedded and Additional Mitigation

NSR ID	NSR Name	Assessment Period	Predicted Rating Level, dB L _{A,r,T} *	Background Sound Level, dB L _{A90}	Difference, dB
NSR01	No. 1 & 2 Edinburgh Road	Daytime	29	52	-23
		Night-time	30	35	-5
NSR02	West Harbour Road	Daytime	27	47	-20
		Night-time	27	36	-9
NSR03	Cockenzie House & Gardens	Daytime	25	47	-22
		Night-time	25	36	-10
NSR04	Hawthorn Terrace	Daytime	30	41	-11
		Night-time	31	29	+2
NSR05	The Antiquaries	Daytime	25	52	-27
		Night-time	27	30	-3
NSR06	Atholl View	Daytime	29	34	-5
		Night-time	33	26	+7
NSR07	Appin Drive	Daytime	25	42	-17
		Night-time	26	26	0
NSR08	Hawthorn Bank	Daytime	27	52	-25
		Night-time	27	35	-8
* Predicted specific sound level (as per Table 6), plus a BS4142:2014 penalty of +5 dB					

- 20 BS4142:2014 states that “the lower the rating level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact” and that “a difference of around +5 dB is likely to be an indication of an adverse impact, depending on the context”.
- 21 This is applicable to NSR06 (Atholl View), whereby the predicted rating level (assuming additional mitigation has been incorporated) is +7 dB above the measured night-time background sound level.
- 22 However, with respect to context, BS4142:2014 goes on to state that “where background sound level and rating levels are low, absolute levels might be as, or more, relevant than the

margin by which the rating level exceeds the background” and that “this is especially true at night”.

- 23 This is applicable at Atholl View (NSR06), as both the night-time background sound level and the predicted night-time rating level are considered to be low, at 26 dB and 33 dB respectively. In this context, an absolute noise limit is considered more appropriate and is in line with the recommendations of BS4142:2014.
- 24 The predicted night-time rating level at Atholl View (NSR06) is 33 dB L_{Aeq} . This predicted level is more than 10 dB below the existing night-time ambient noise level at this location which is 44 dB L_{Aeq} . A difference of 10 dB or more is an indication that the predicted night-time operational noise would not increase the existing night-time ambient noise¹. Therefore, with regards to the highest (external) predicted rating level of 33 dB L_{Aeq} (at Atholl View during the night-time period), this is unlikely to be significant in the context of the existing night-time noise levels.
- 25 Furthermore, and assuming 15 dB attenuation through a partially open window², it can be concluded that the resulting internal night-time noise levels would be comfortably below the BS8233:2014 recommended noise limit of 30 dB L_{Aeq} (i.e. $44 - 15 = 29$ dB).
- 26 The 1999 WHO guidelines also refer to an internal night-time noise limit of 30 dB L_{Aeq} in the context of night-time exposure to noise and sleep disturbance. The guidelines state that *“if negative effects on sleep are to be avoided the equivalent sound pressure level should not exceed 30dB(A) indoors for continuous noise”*. Again, it can be concluded that this recommended internal night-time noise limit would be achieved, based on the predicted rating levels in Table 7 and with reference to the existing night-time ambient noise level.
- 27 With reference to maximum (or peak) noise levels associated with the operation of the Onshore Substation, this assessment presents the highest ambient noise levels expected – corresponding to all components operating simultaneously and continuously. The operation of the Onshore Substation is not anticipated to generate ‘one-off’ or ‘individual’ noise events, and as such, the associated noise levels are likely to be constant.

3D.2.2 Conclusion

- 28 To conclude, it has been shown that for the majority of the closest receptors, the predicted operational noise levels (without the earth bund) do not exceed the measured background noise levels. This is applicable during both the daytime and night-time periods, and is based on the incorporation of noise mitigation measures into the design of the Onshore Substation. Where noise levels are predicted to be above the background noise level (at night-time at NSR04), this is predicted to be no more than +5 dB, and therefore unlikely to have an adverse impact in accordance with the guidance of BS4142:2014.
- 29 At Atholl View (NSR06), the predicted operational noise level is predicted to be +7 dB above the measured background noise level at night-time; however, the predicted level is within appropriate absolute night-time limits for the protection of sleep disturbance. Effects from operational noise are therefore assessed as not significant.

¹ Due to logarithmic addition of decibels, whereby $44 \text{ dB} + 33 \text{ dB} = 44 \text{ dB}$

² BS8233:2014, Annex G.1, *“if partially open windows were relied upon for background ventilation, the insulation would be reduced to approximately 15 dB”*.

3D.3 Landscape Assessment

3D.3.1 Impacts

- 30 ELC has requested that the EIA Report for the OnTW assesses the potential effects of the OnTW in the event that the earth bund located to the south of the Application Site (north of Atholl View) is not in place. This steep earth mounding with grass cover was put in place when the housing on the north east edge of Prestonpans (a short section of Appin Drive and part of Atholl View) was built in order to provide residents with screening of the former Cockenzie Power Station.
- 31 If the bund were to be removed, it would open up views for the housing on the north side of Atholl View and a short section of housing on the south side of Appin Drive between Nethershot Road and Appin Drive. Rather than the existing short distance views of the grassed bund, views from houses at these locations would be obtained across the B1348 (Edinburgh Road) towards the informal recreation area on Preston Links with the Application Site at approximately between 225 metres and 450 metres further to the north, north east.
- 32 The OnTW LVIA assessed effects on landscape character and visual amenity at Viewpoints 5 and 6 which are located to the south west of the Application Site. Viewpoint 5 is on Edinburgh Road and Viewpoint 6 is located on the top of the bund providing elevated and open views across Onshore Substation (see *Appendix 8C: Viewpoint Assessment*).
- 33 At Viewpoint 5, on the edge of the urban area, the predicted magnitude of change from the Onshore Substation is assessed as being slight due to the limited visibility as a consequence of intervening existing mounds at Preston Links as well as the embedded landscape mitigation mounds and related planting within the Application Site. This will result in a Moderate/Minor effect for the medium sensitivity landscape character of the urban area; and a Moderate effect for high sensitivity visual amenity receptors (see *Appendix 8C: Viewpoint Assessment* and *Appendix 8B: Figure 8.11*). Both the effect on landscape character and visual amenity are not significant.
- 34 Viewpoint 6 is slightly further to the south west and located on the elevated bund. It is considered representative of the Coastal Margins Landscape Character Area of medium sensitivity, and recreational walkers, of high sensitivity, who follow the informal footpath on top of the bund. The magnitude of change arising from the OnTW at Viewpoint 6 is assessed as substantial, resulting in a Major/ Moderate effect on landscape character and a Major effect for recreational walkers, both being significant effects (see *Appendix 8C: Viewpoint Assessment* and *Appendix 8B: Figure 8.12*).
- 35 Removal of the existing steep sided grassed bund would open up views for residents of the houses on the north east edge of Prestonpans across the informal open space area at Preston Links and towards the Firth of Forth with the hills of Fife on the opposite shore. The Onshore Substation would form an element of this view, seen in the context of the existing Cockenzie substation at a similar distance, which it would resemble in terms of building material and colour. Depending on when the bunding were to be removed in relation to the construction of the OnTW, the embedded mitigation of earth mounding and associated planting within the Application Site will be established and will provide some screening of the lower elements of the Onshore Substation. The Onshore Substation will not obscure views across Preston Links towards the Firth of Forth which would be opened up by removal of the bund, but it would

form a built element seen alongside the existing Cockenzie substation to the right hand side of views north, north eastward.

- 36 As demonstrated by comparison of the visualisations for the LVIA representative Viewpoints 5 and 6, the magnitude of change for receptors on this north edge of Prestonpans is likely to vary dependent upon the extent to which the existing earth mounds on Preston Links recreation area on the north side of the B1348 (Edinburgh Road) as well the proposed embedded mitigation associated with the Onshore Substation intervene in views from this area.

3D.3.1 Conclusion

- 37 Accordingly, if the existing bunding around Atholl View were to be removed, it is considered that for high sensitivity residents on the two sections of road at Appin Drive and Atholl View in Prestonpans with views towards the Onshore Substation, the magnitude of change could vary between substantial and slight depending on the angle of view and intervening landforms. This would result in Major and significant to Moderate and not significant effects on visual amenity for the small number of residents at this north east edge of Prestonpans.

3D.4 Conclusion

- 38 To conclude this appendix details the results of a noise and visual assessment of the potential impacts associated with the operation of the OnTW, assuming that the earth bund located to the south of the Application Site (north of Atholl View) is not in place.
- 39 The noise assessment has shown that there are no significant effects associated with the operation of the OnTW without the earth bund.
- 40 The visual assessment has concluded that if the existing bunding around Atholl View were to be removed, there is the potential for Major and significant to Moderate and not significant effects on visual amenity for the small number of residents at this north east edge of Prestonpans.